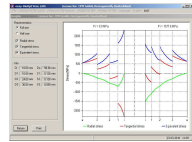
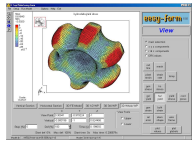
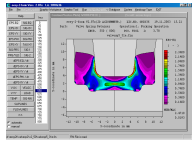


“The Use of Simulation to predict Tool Failure in Cold Forging Processes“

*Dr. Gerhard H. Arfmann, Dr. Michael Twickler
CPM GmbH, Herzogenrath, Germany*



Why to study FEA applications in metal forming processes under the aspect of tool failure?

Motivation:

The prediction of tooling failure is not a standardized application of simulation in industry.

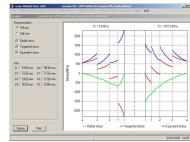
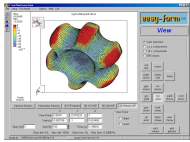
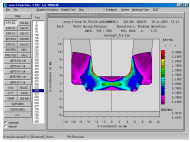
Successful applications had to be studied to find out guidelines to support the design engineer.

By getting experience from these studies rules should be given to enable the design engineer to foresee problems in future and therefore avoid costs and development time.

The design engineer shall be enabled to develop long lasting tooling by using simulation instead of costly trial and error procedures.

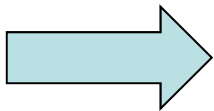
The study focused on real applications in industry to give most practical guidelines.

The presentation shows such successful industrial applications.

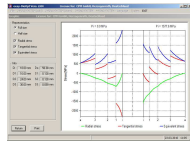
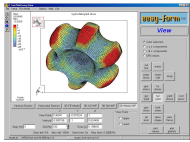
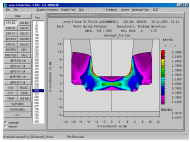


Die failure in a multi station cold forming process

The customer faced severe tool failure in operation four of a five station process.



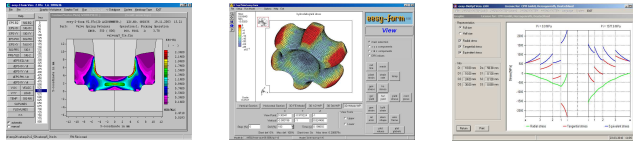
What can be optimized to get better tool life?



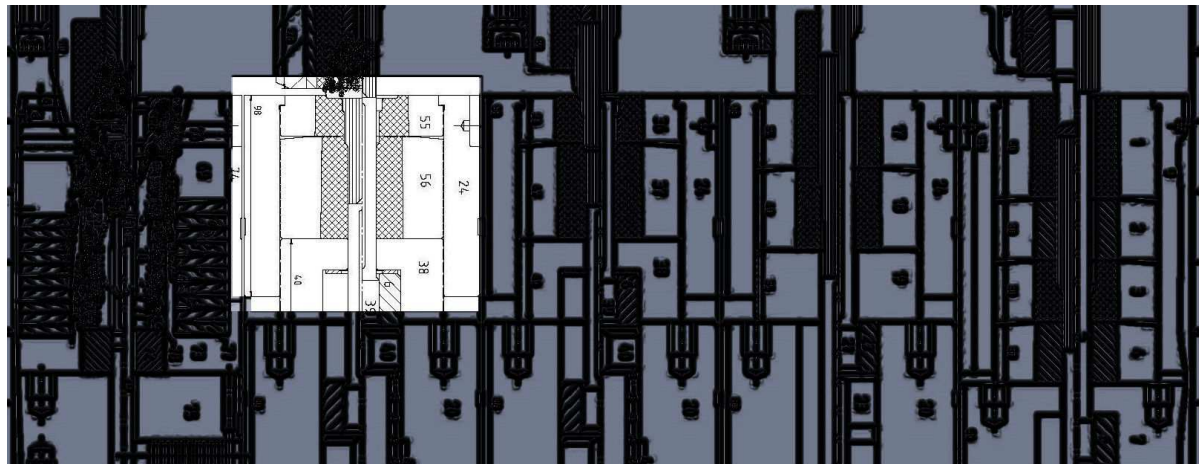
Die failure in a multi station cold forming process



The five station
cold forging
process

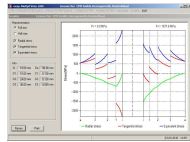
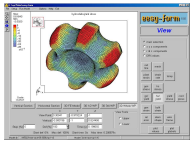
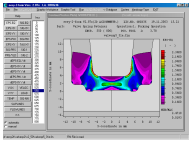


Die failure in a multi station cold forming process

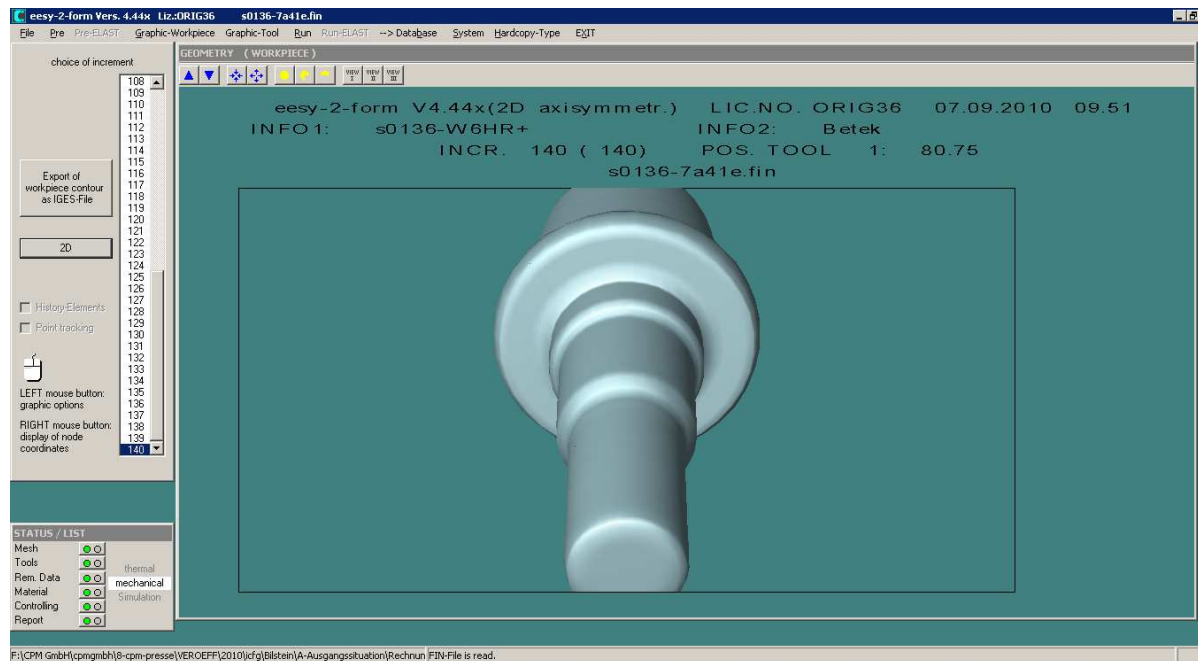


The five station
cold forging
process

Initial tool design in operation 4

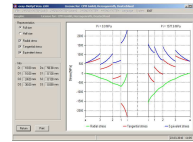
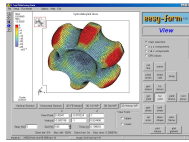
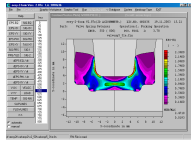


Die failure in a multi station cold forming process



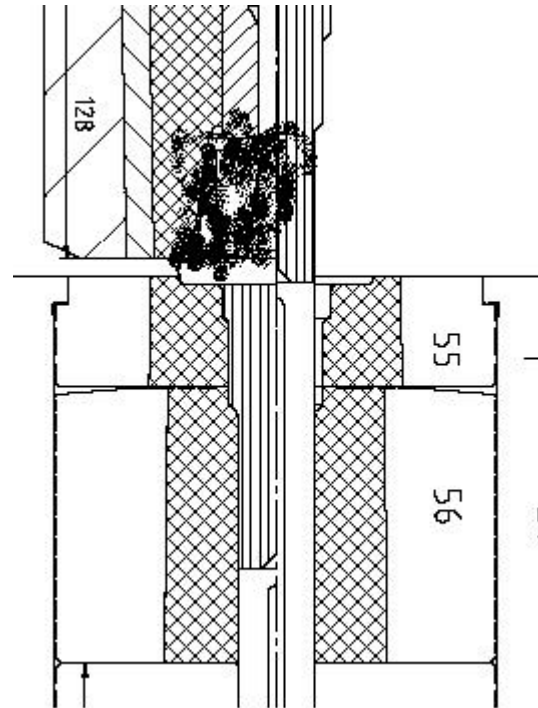
The five station
cold forging
process

Forming in operation 4

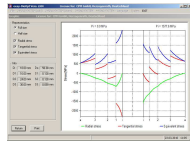
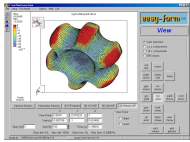
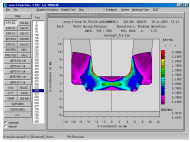


Die failure in a multi station cold forming process

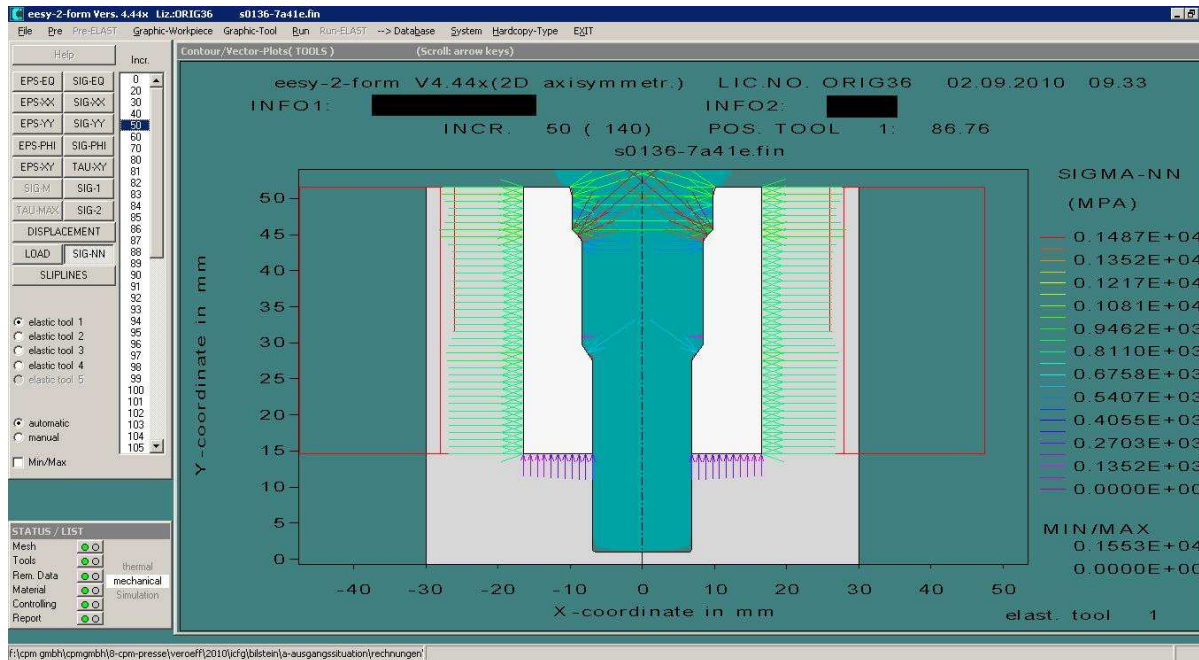
Initial design
of the
die in
operation 4
(carbide – pre
stressed with
a single ring)



The five station
cold forging
process

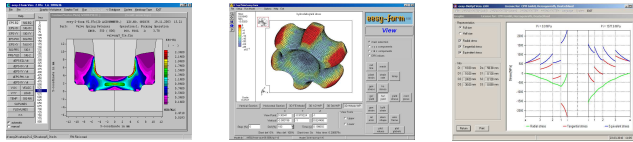


Die failure in a multi station cold forming process

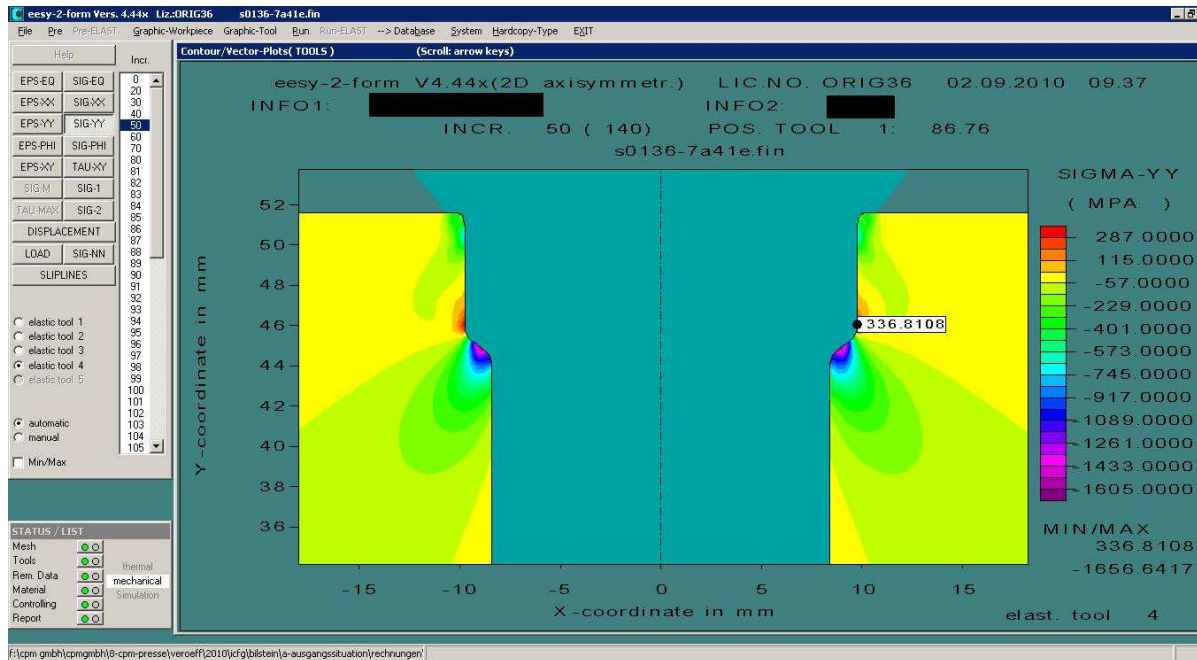


The five station
cold forging
process

Pressure on the carbide

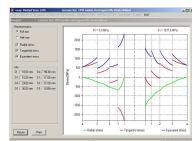
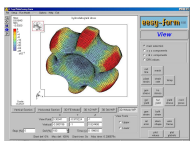
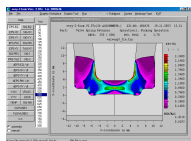


Die failure in a multi station cold forming process



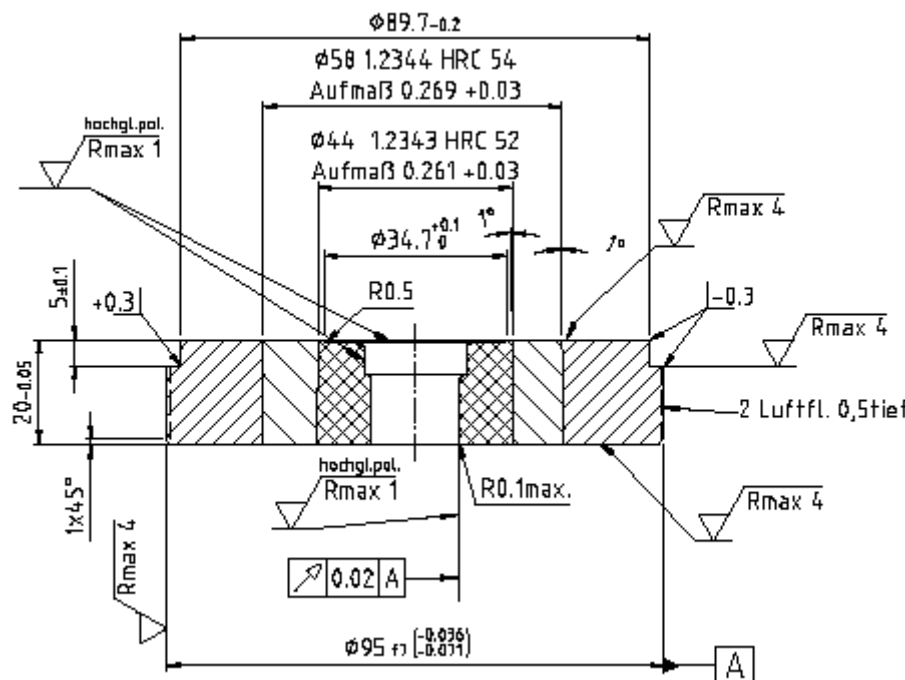
The five station
cold forging
process

Positive axial stress in the carbide => tool failure

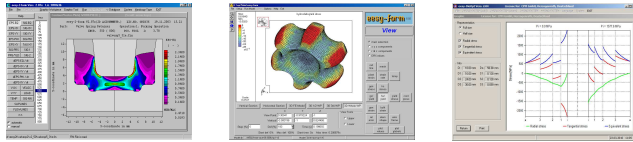


Die failure in a multi station cold forming process

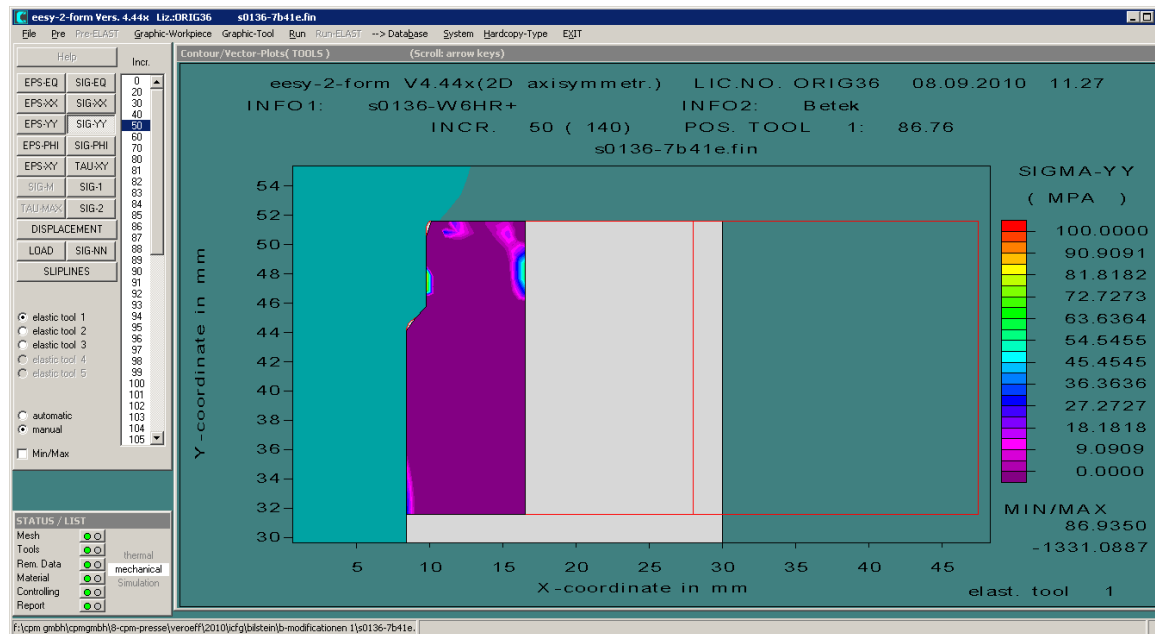
new design
of the
die in
operation 4
(carbide split –
pre
stressed with
two rings)



The five station
cold forging
process

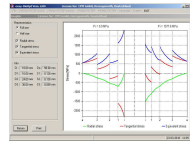
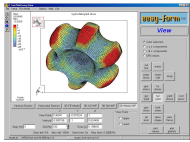
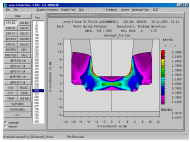


Die failure in a multi station cold forming process



The five station
cold forging
process

Still positive axial stress in the carbide => tool failure

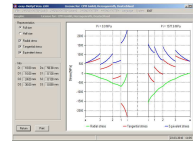
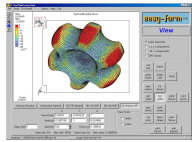
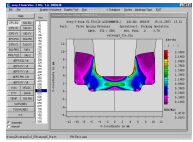


Die failure in a multi station cold forming process



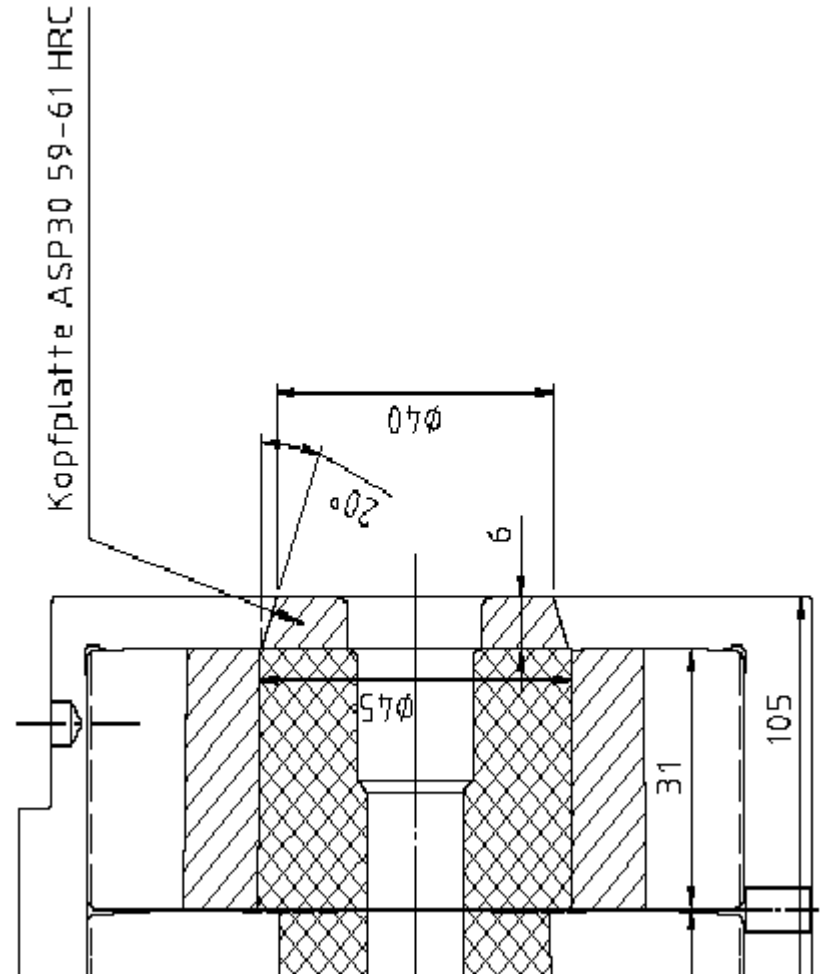
The five station
cold forging
process

Tool breakage persists

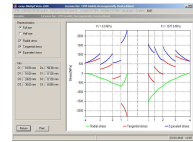
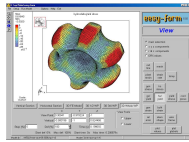
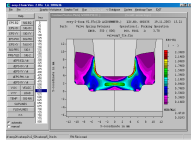


Die failure in a multi station cold forming process

new design idea
of the die in
operation 4
(Disc made of
ASP 30 – carbide
pre stressed with
two rings)

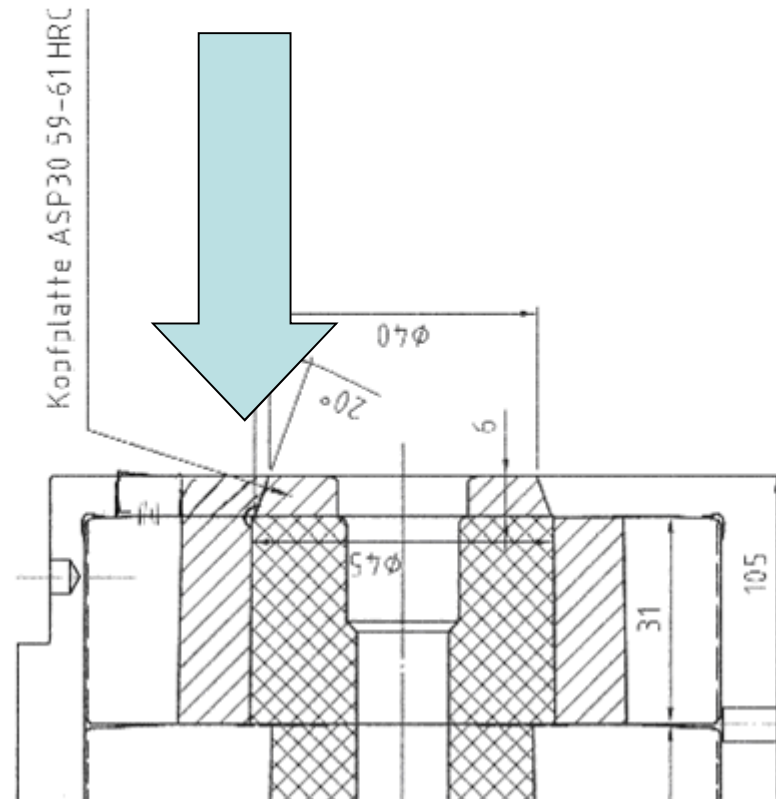


The five station
cold forging
process

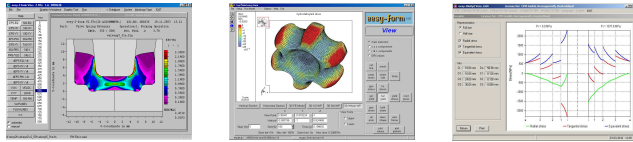


Die failure in a multi station cold forming process

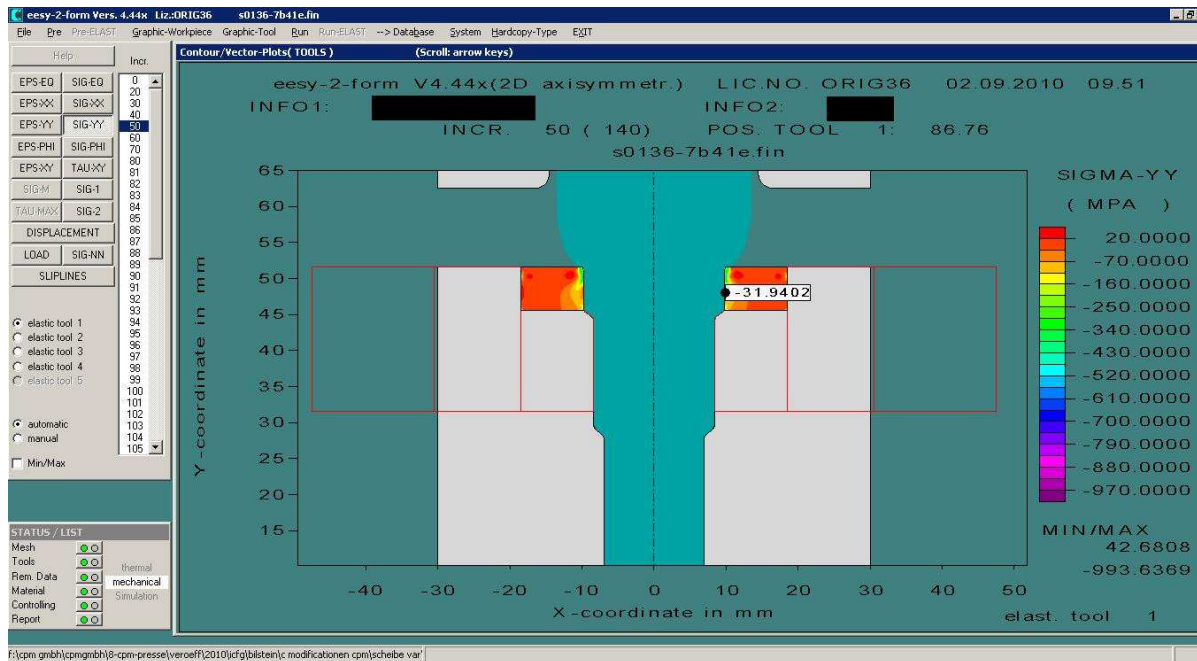
corrected
new design
of the die in
operation 4
(Disc made of
ASP 30 – carbide
and disk pre
stressed with
two rings)-
corrected by
toolmaker



The five station
cold forging
process

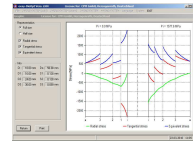
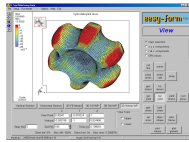
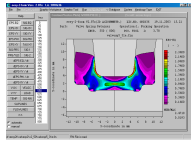


Die failure in a multi station cold forming process



The five station
cold forging
process

Simulation shows compressive stress
- tool life increased from 1.000 to 25.000 pieces



Die failure in a multi station cold forming process

Result:

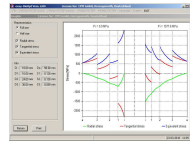
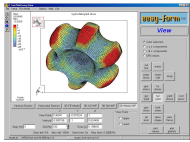
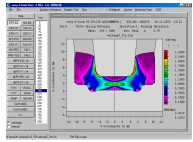
Systematic analysis of the various design ideas leads to better tool design and better understanding of the design.

Testing on the machine can be avoided.

Design rules could be reviewed.

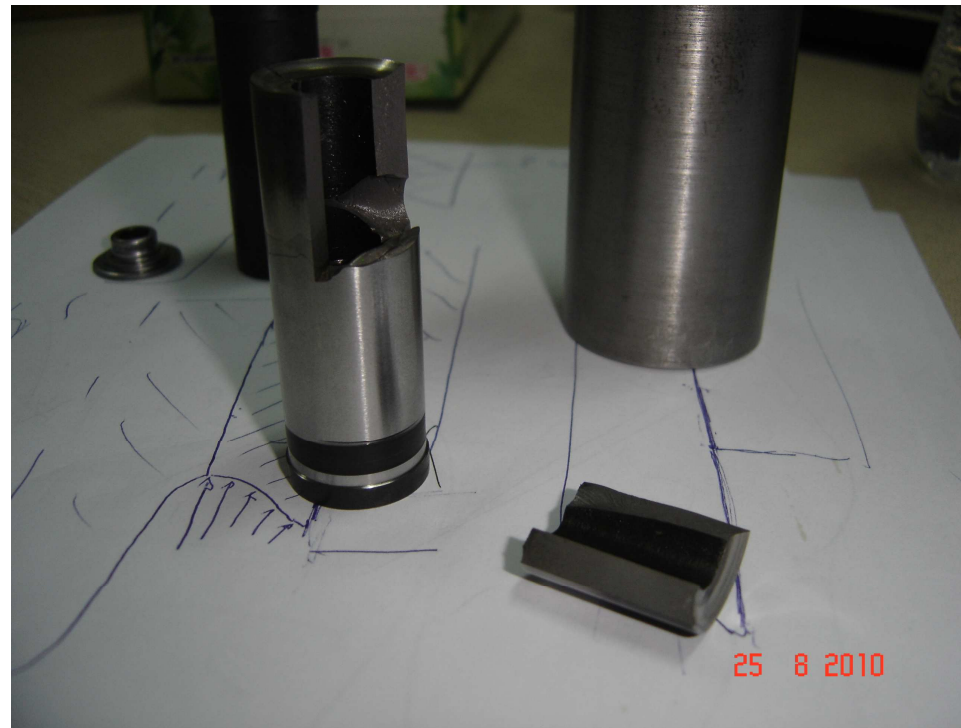
Future designs can be made better by using FEA from the beginning and considering the new design rules.

The five station
cold forging
process

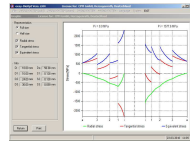
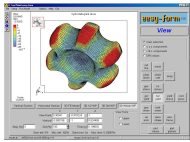
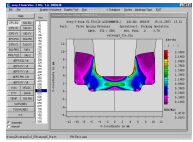


Punch failure in a multi station process

Punches of
operation 5
fail premature



Five station
cold forging
process to
form a
valve spring
retainer

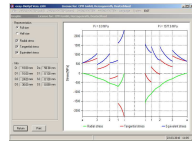
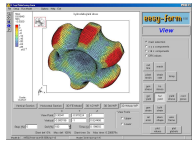
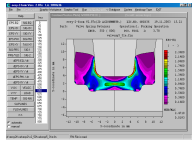


Punch failure in a multi station process

Punches of
operation 5
fail premature



Five station
cold forging
process to
form a
valve spring
retainer

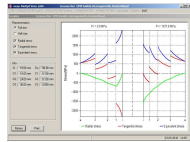
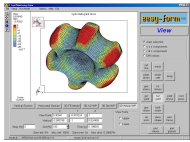
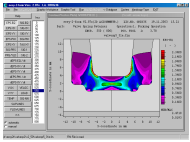


Punch failure in a multi station process

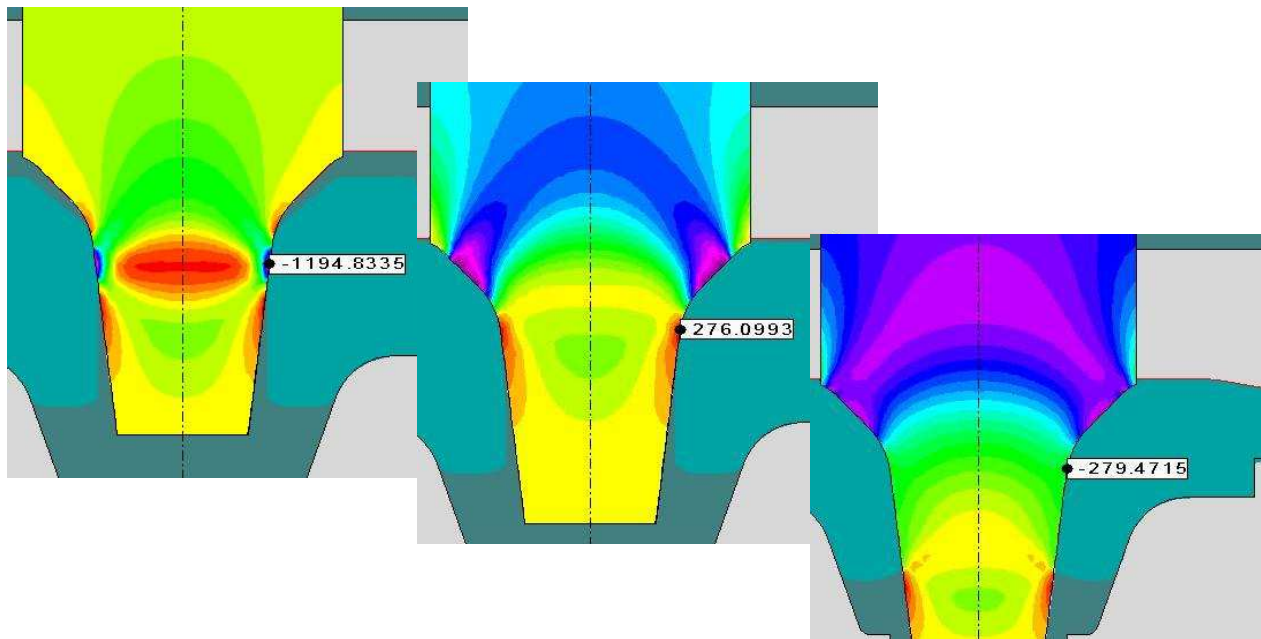
Punches of
operation 5
fail premature



Five station
cold forging
process to
form a
valve spring
retainer



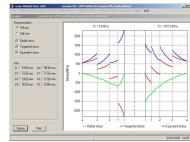
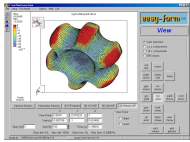
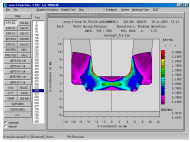
Punch failure in a multi station process



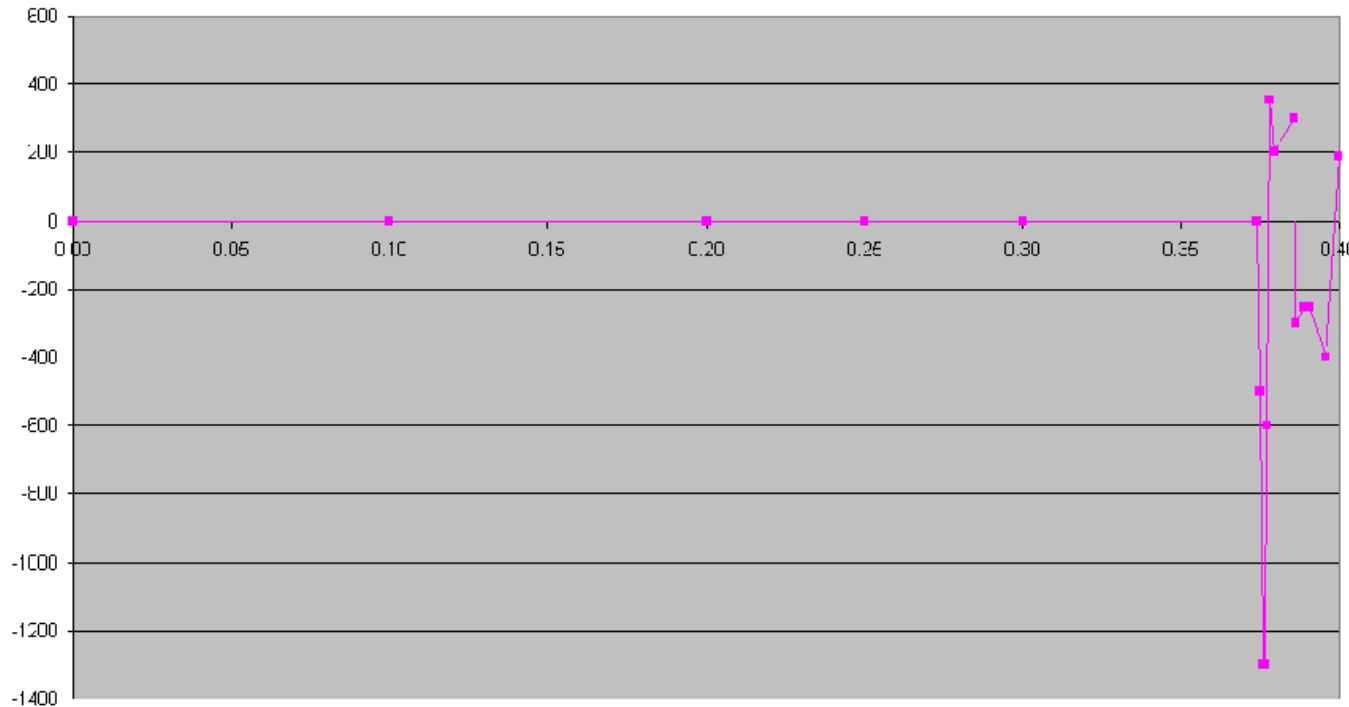
Five station
cold forging
process to
form a
valve spring
retainer

Alternating Stress

Failure due to fatigue



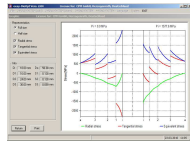
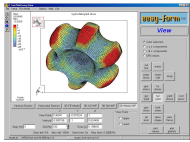
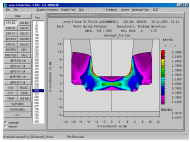
Punch failure in a multi station process



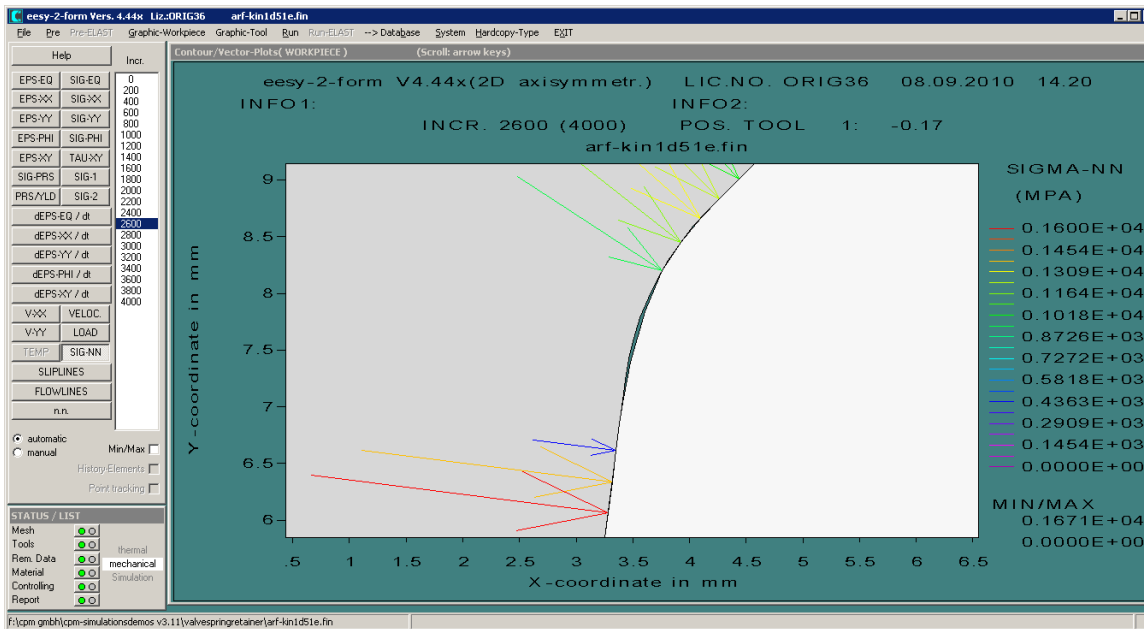
Five station
cold forging
process to
form a
valve spring
retainer

Alternating Stress in short time period

Failure due to fatigue

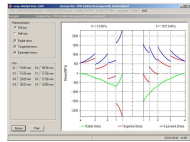
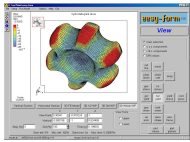
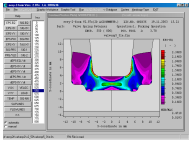


Punch failure in a multi station process

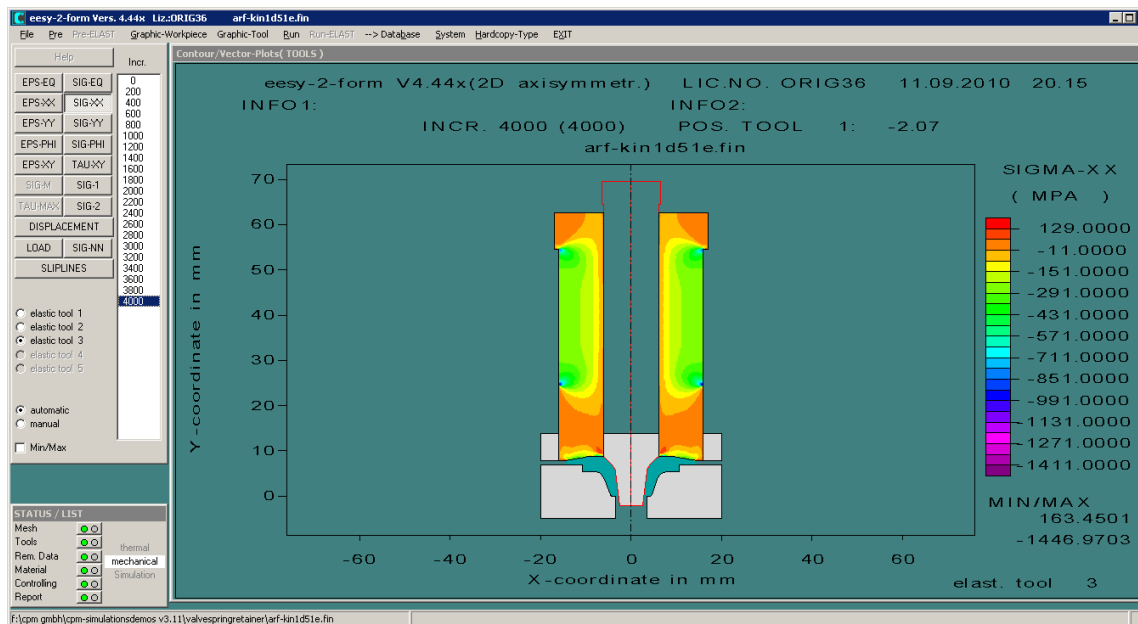


Five station
cold forging
process to
form a
valve spring
retainer

Reason for failure: material lost contact to the tooling

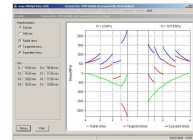
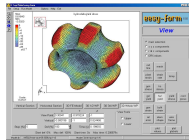
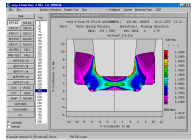


Punch failure in a multi station process

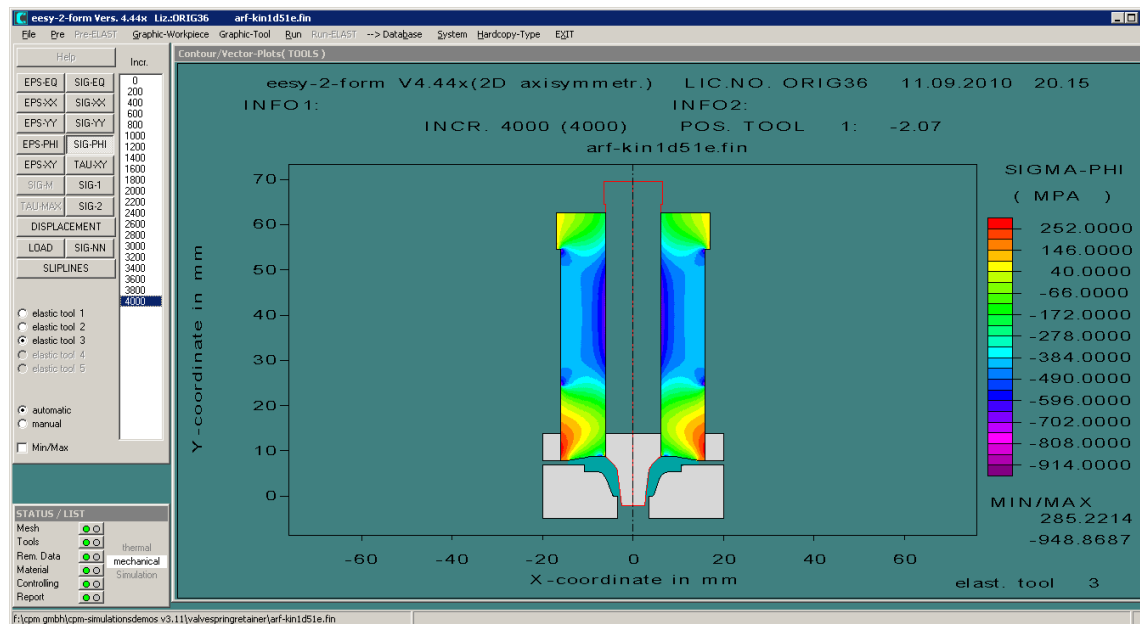


Five station
cold forging
process to
form a
valve spring
retainer

High stress concentration at the point of breakage (Sig xx)

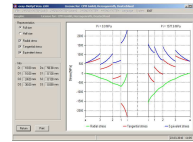
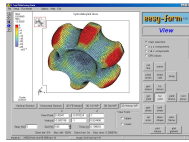
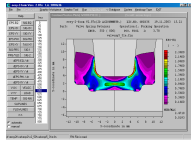


Punch failure in a multi station process



Five station
cold forging
process to
form a
valve spring
retainer

positive tangential stress below the point of breakage

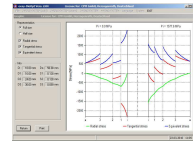
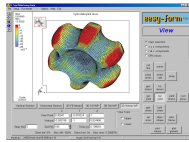
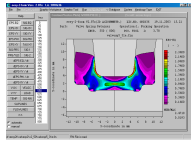


Punch failure in a multi station process

Crack initialization



Five station
cold forging
process to
form a
valve spring
retainer



Punch failure in a multi station process

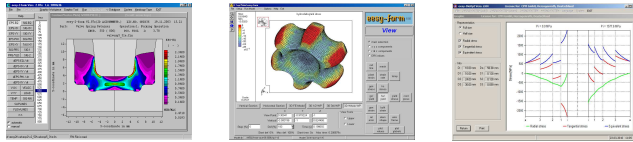
Result:

The change of the progression design to get the material in contact to the pin during all the process solved the problem.

A longer housing of the punch to avoid the upsetting in the front solved the problem.

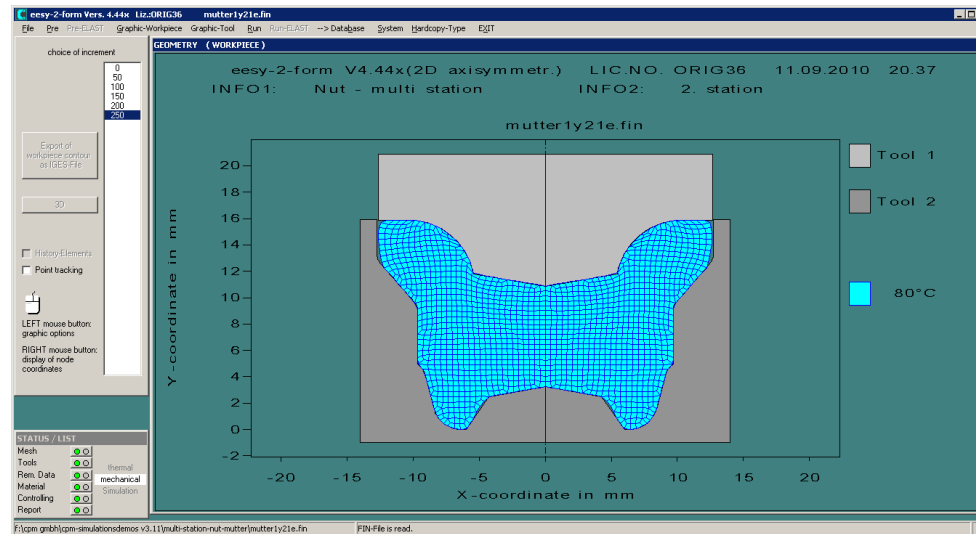
Related design rules could be reviewed.

Five station
cold forging
process to
form a
valve spring
retainer

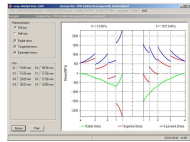
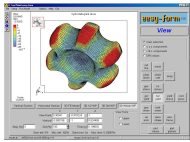
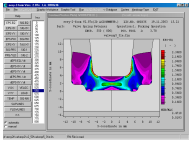


Punch failure in a multi station process

Punch of
operation 3
fails

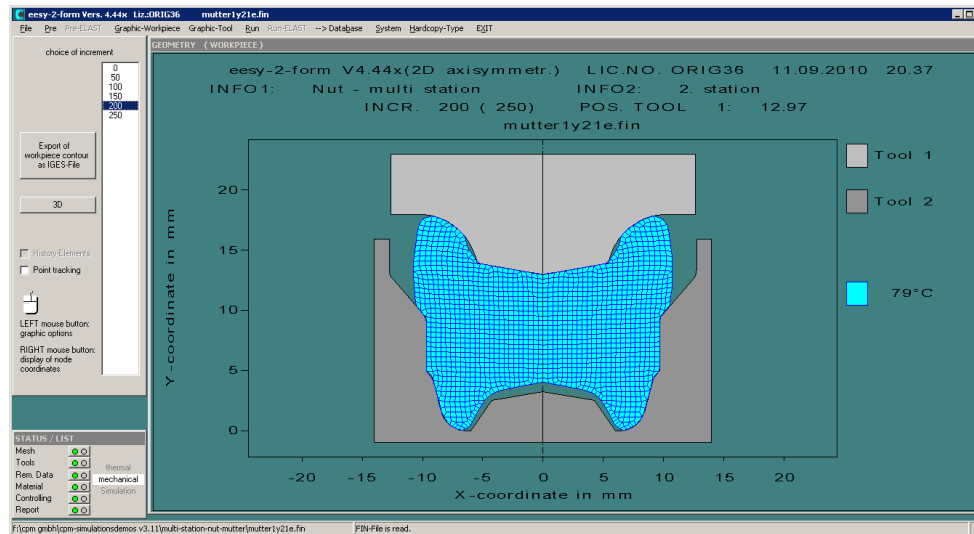


Nut making
cold forging
process

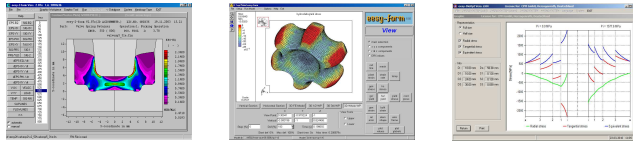


Punch failure in a multi station process

Punch of
operation 3
fails

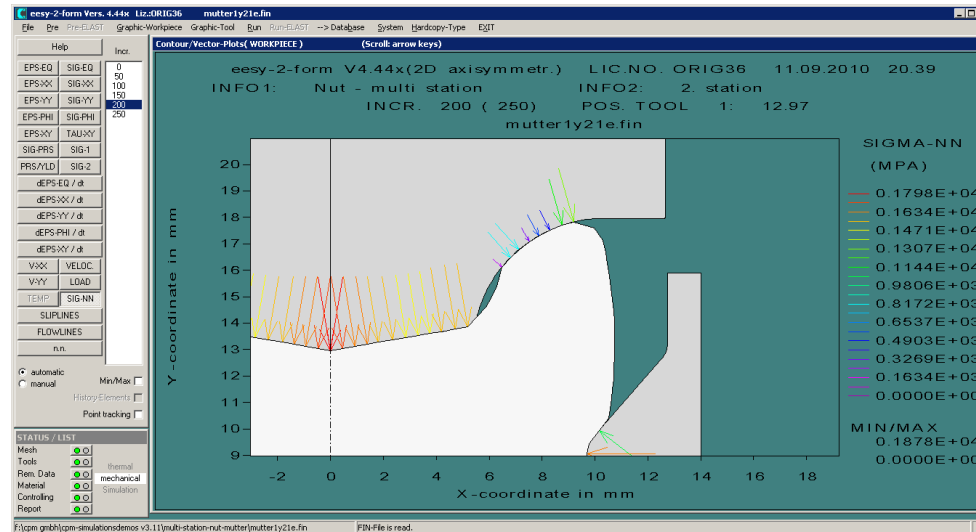


Nut making
cold forging
process



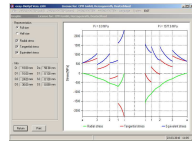
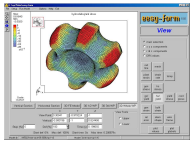
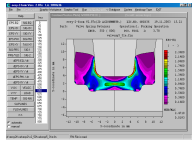
Punch failure in a multi station process

Material flow
causes severe
stress
distribution



Nut making
cold forging
process

Result: positive stress in the punch -> punch failure



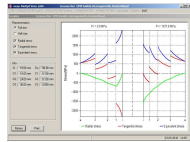
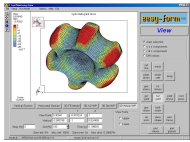
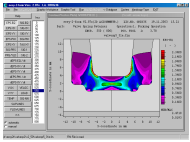
Punch failure in a multi station process

Material flow
causes severe
stress
distribution



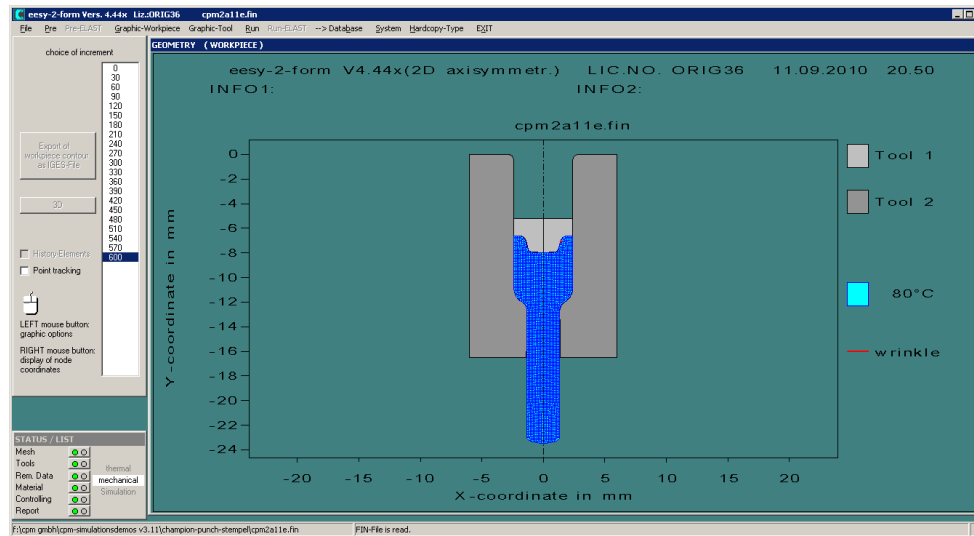
Nut making
cold forging
process

Result: positive stress in the punch -> punch failure

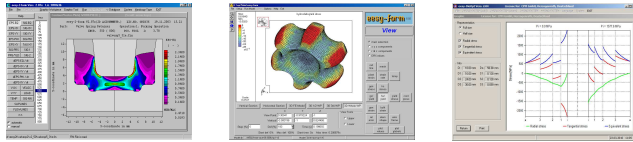


Punch failure in extrusion process

Punch of
operation 2
fails

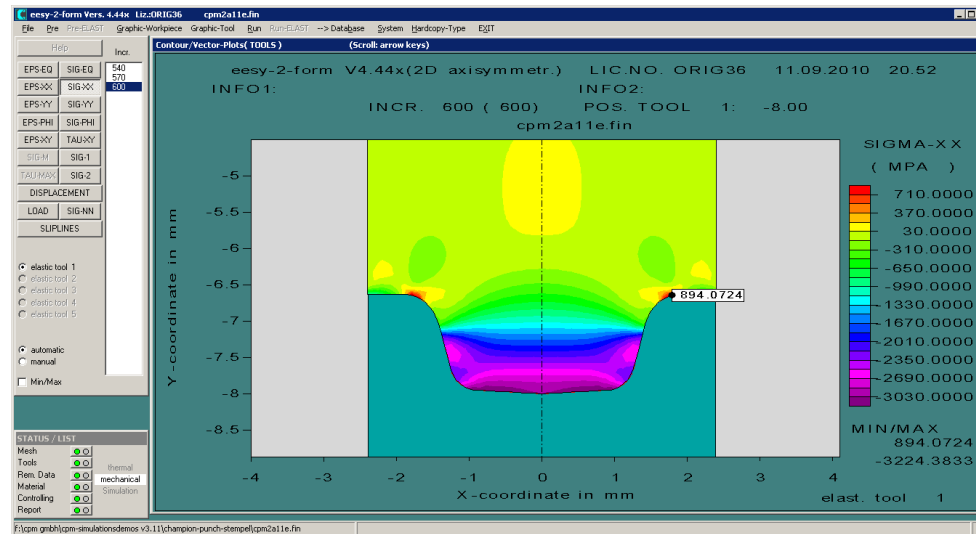


Cold forging
extrusion
process



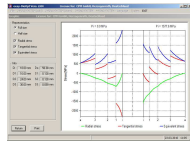
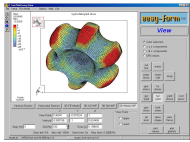
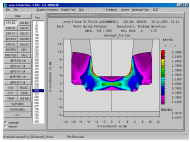
Punch failure in extrusion process

Punch of
operation 2
fails



Cold forging
extrusion
process

High local positive radial stress -> punch failure



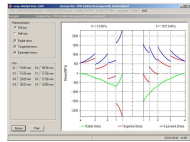
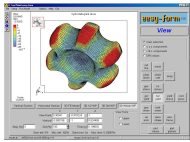
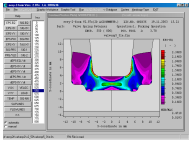
Punch failure in extrusion process

Punch of
operation 2
fails



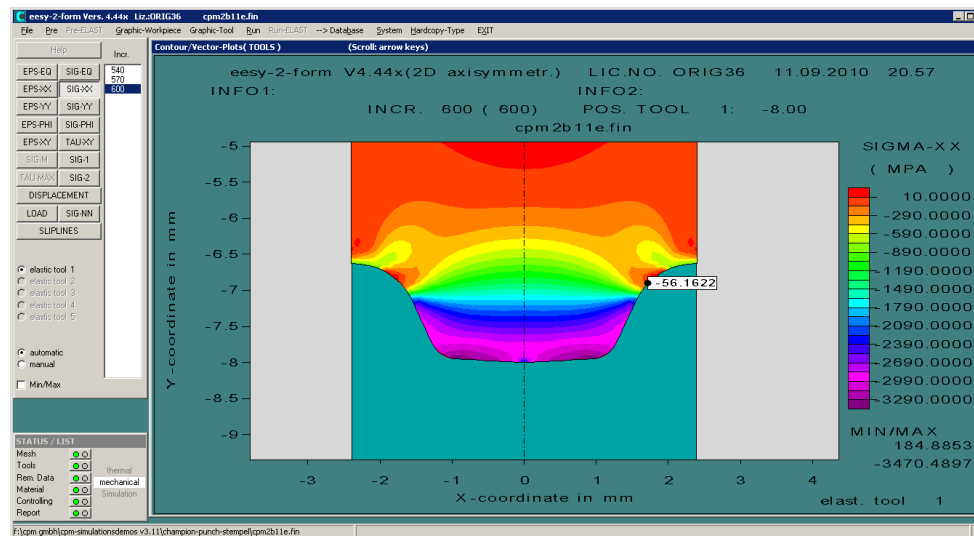
Cold forging
extrusion
process

Picture of a similar failure (picture from ICFG)



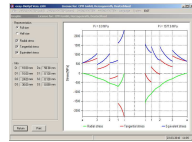
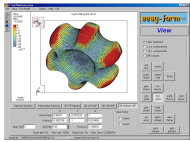
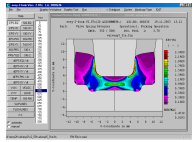
Punch failure in extrusion process

Punch of
operation 2
changed



Cold forging
extrusion
process

No high local positive radial stress after change of radius

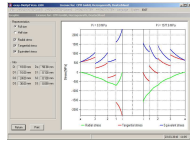
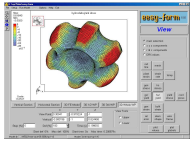
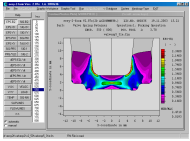


Die failure in extrusion Using a hybrid approach to optimize the tool design

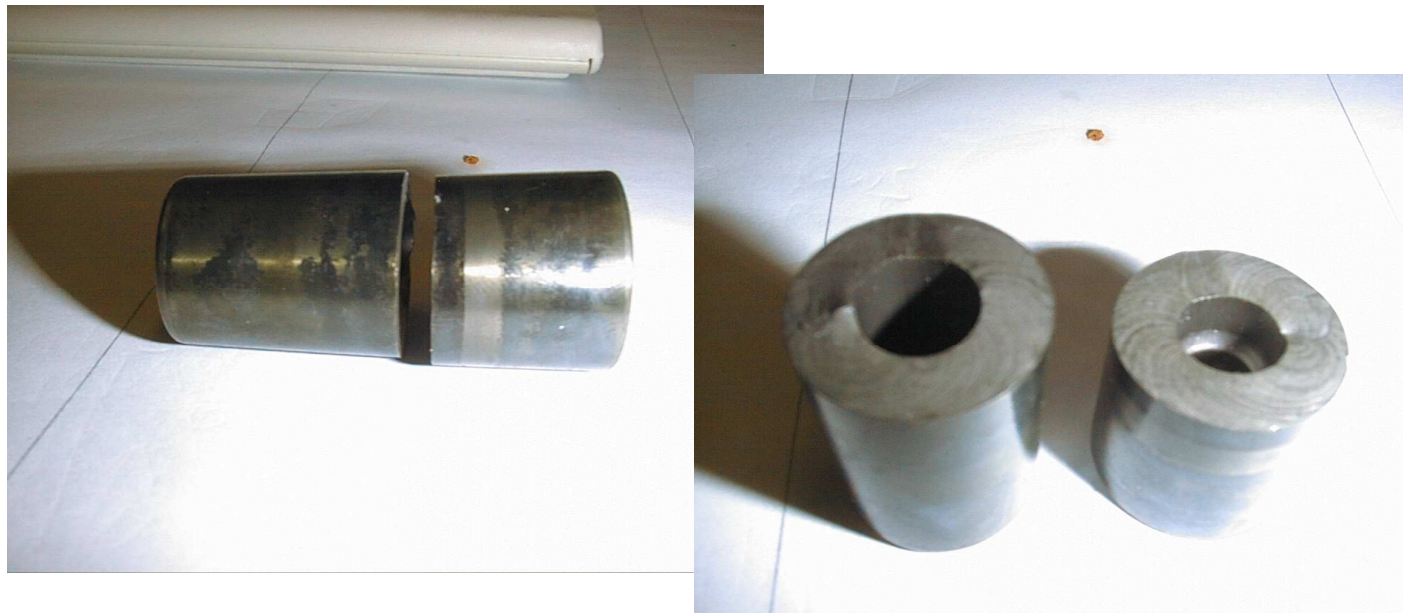


Cold forging
extrusion
process

Die failure mainly due to overloading

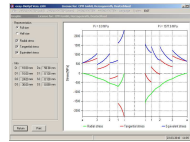
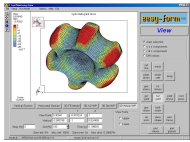
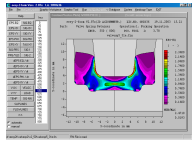


Die failure in extrusion Using a hybrid approach to optimize the tool design

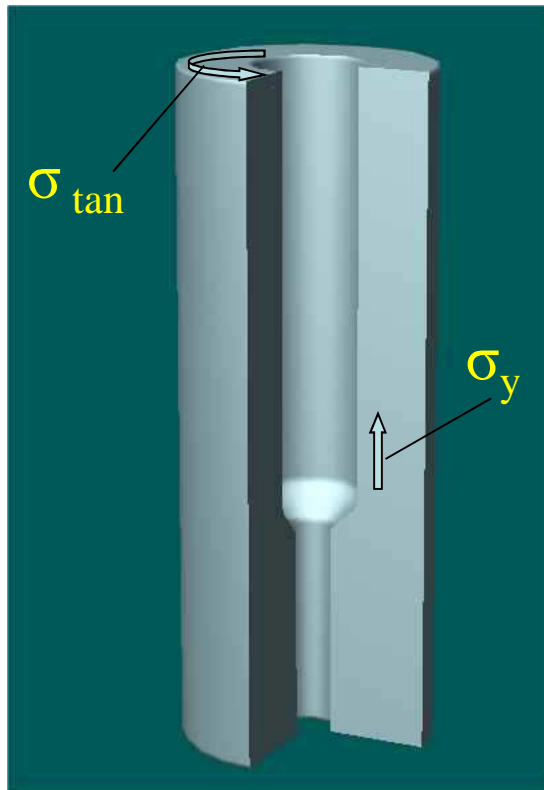


Cold forging
extrusion
process

Die failure mainly due to axial stress in the insert



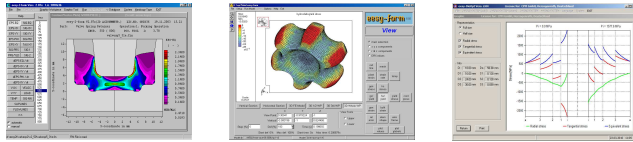
Die failure in extrusion Using a hybrid approach to optimize the tool design



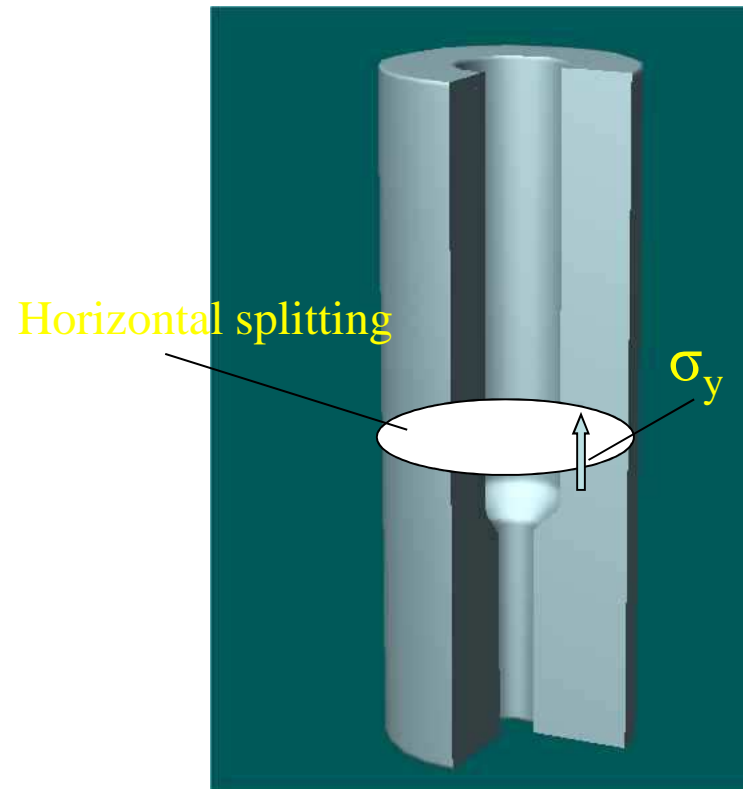
σ_{tan} : critical for axial
cracks

σ_y : critical for
horizontal cracks

Cold forging
extrusion
process



Die failure in extrusion Using a hybrid approach to optimize the tool design

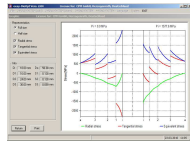
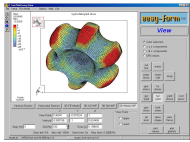
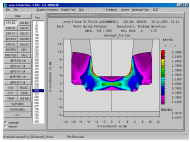


σ_y : critical for
horizontal breackage

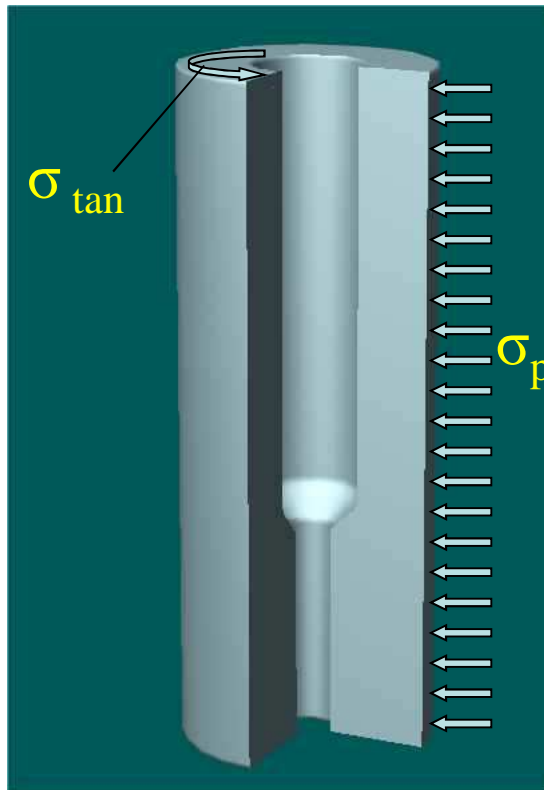
⇒ splitt the insert

Cold forging
extrusion
process





Die failure in extrusion Using a hybrid approach to optimize the tool design

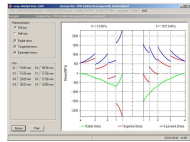
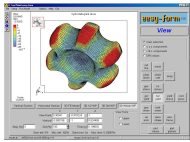
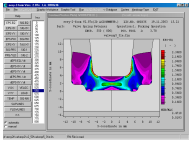


σ_{\tan} : critical for
radial cracks

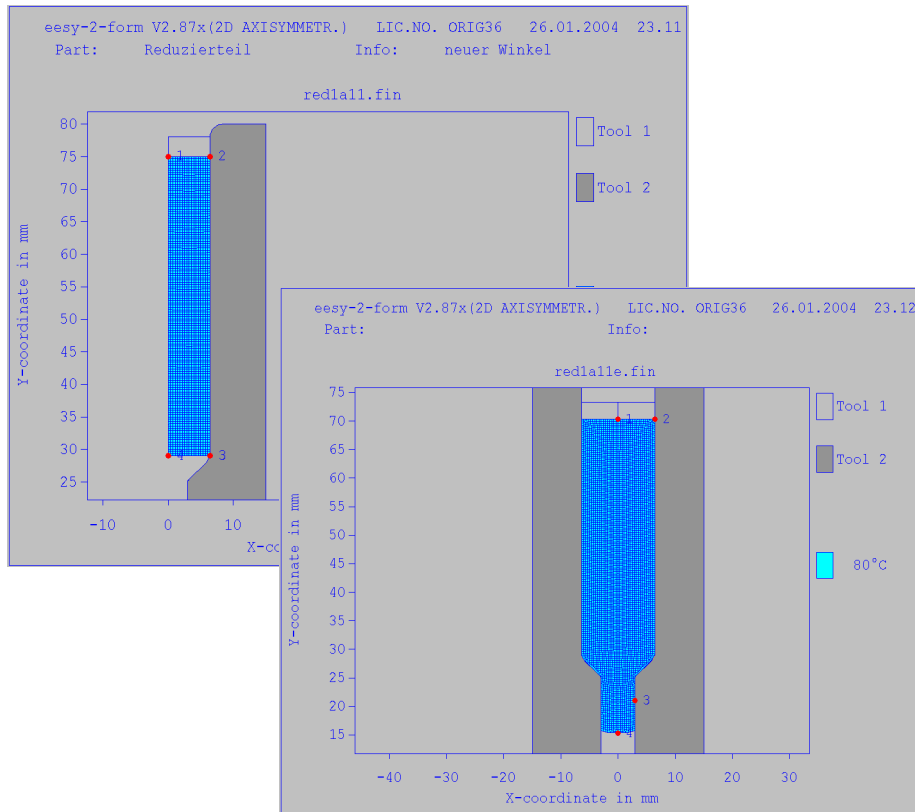
⇒ pre-stress the insert

Cold forging
extrusion
process



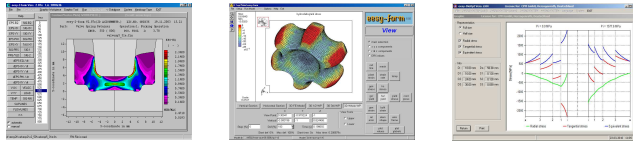


Die failure in extrusion Using a hybrid approach to optimize the tool design

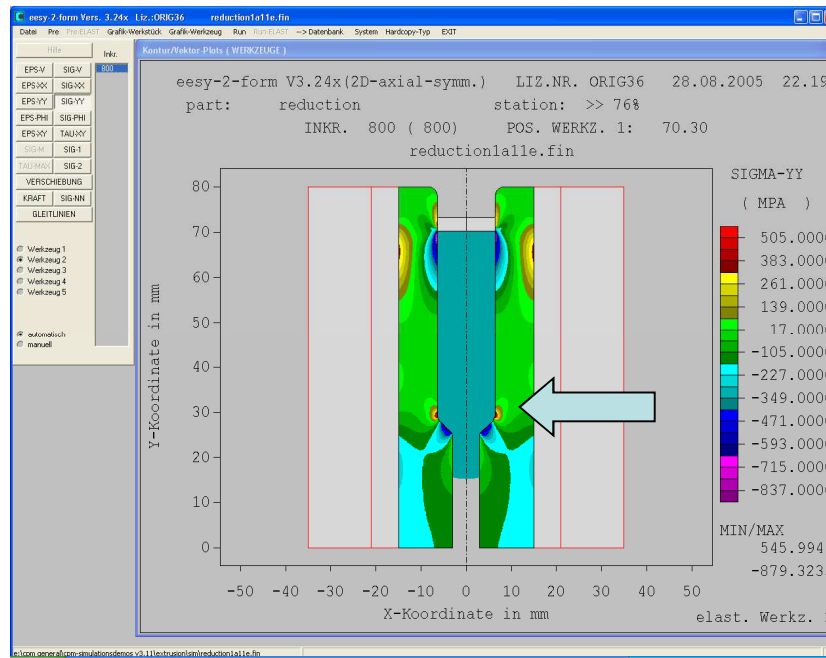


Process
material flow

Cold forging
extrusion
process

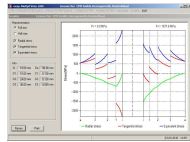
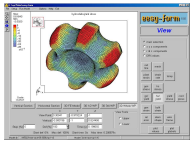
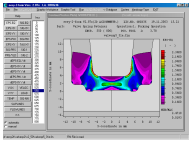


Die failure in extrusion Using a hybrid approach to optimize the tool design

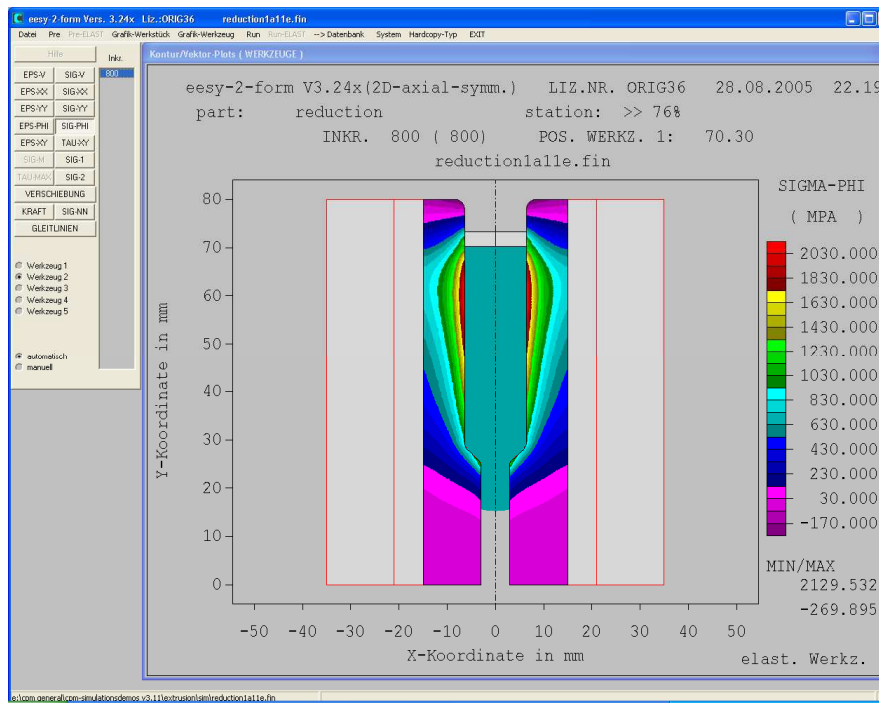


Cold forging
extrusion
process

Axial stress in the insert => split the carbide insert

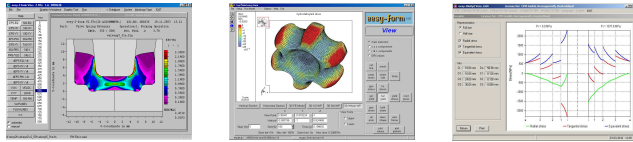


Die failure in extrusion Using a hybrid approach to optimize the tool design

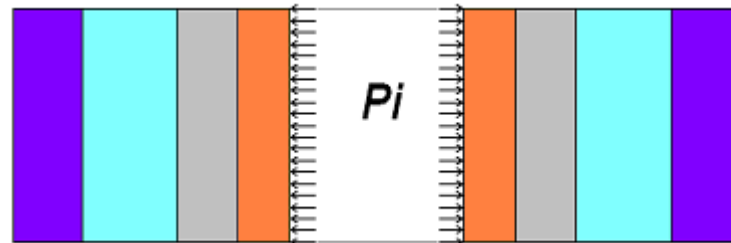


Cold forging
extrusion
process

High tangential stress => improve the pre-stressing

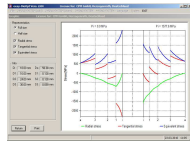
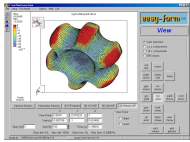
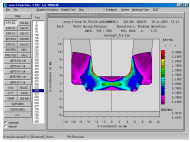


Die failure in extrusion Using a hybrid approach to optimize the tool design



Cold forging
extrusion
process

Simplified pre-stress analysis to optimize the design



Die failure in extrusion Using a hybrid approach to optimize the tool design

easy-DieOpt Vers. 1.95 Lizenz für: CPM GmbH, Herzogenrath, Deutschland

Datei 2-RING-SYSTEM (kalt) 2-RING-SYSTEM (warm) 3-RING-SYSTEM 4-RING-SYSTEM Sprache System EXIT

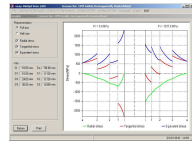
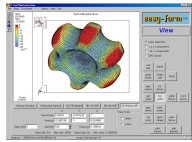
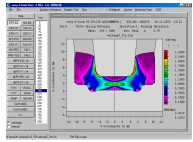
3-RING-SYSTEM Lizenz für: CPM GmbH, Herzogenrath, Deutschland

	Einsatz	1. Schrupftring	2. Schrupftring
Innendurchmesser Di	10.00 mm		
Aussendurchmesser Da	40.00 mm		
Fugendurchmesser D1	15.00 mm		
Schrumpfmaß S1	0.109 mm		
Fugendurchmesser D2	26.00 mm		
Schrumpfmaß S2	0.093 mm		
Innendruck Pi	1298.0 MPa		
Fugendruck P1	937.4 MPa		
Fugendruck P2	382.0 MPa		
Konus-Winkel (für D1)	1.0 °		
Pressweg	3.12 mm		
Werkstoffname	G55	X40CrMoV51	X40CrMoV51
Werkstoffnummer		1.2344	1.2344
E-Modul [MPa]	450000.	216000.	216000.
Poisson'sche Zahl [-]	0.25	0.28	0.28
Zugfestigkeit [MPa]		2050.0	1670.0
Streckgrenze [MPa]		1850.0	1470.0
Anlasstemperatur [°C]		520.	600.
Vergleichsspannung [MPa]	1298.0	1665.0	1323.0
Tangentialspannung [MPa]	0.0	727.6	941.0
Verengung (·) / Aufweitung (*):	von Di 0.007 mm	von Da 0.104 mm	
Zusammenbau	<input checked="" type="radio"/> (2.Schrumpftring + 1.Schrumpftring) ← Einsatz <input type="radio"/> (Einsatz + 1.Schrumpftring) → 2.Schrumpftring <input type="radio"/> Ohne Zwischenbearbeitung		

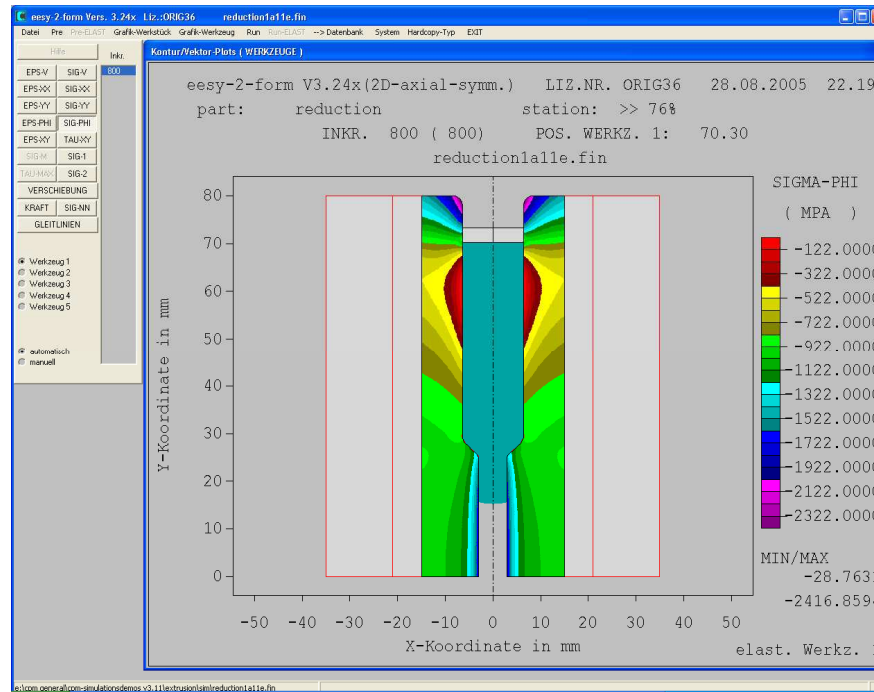
Neu Berechnung Optimierung (Schrumpfmaß) Optimierung (Gesamt) Optimierung (nur D2) Hilfe Grafik

Cold forging
extrusion
process

Simplified pre-stress analysis to optimize the design

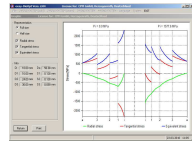
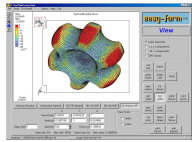
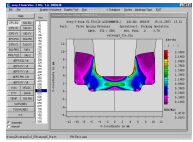


Die failure in extrusion Using a hybrid approach to optimize the tool design



Cold forging
extrusion
process

Checking the optimized design in FEA

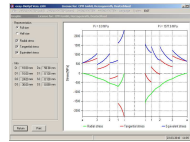
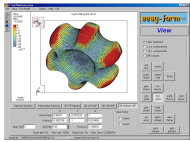
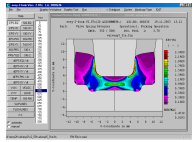


Study of FEA applications in metal forming

Conclusion



A lot of tooling problems can be solved or avoided by consequent use of FEA during the design stage



Why to study FEA applications in metal forming processes under the aspect of tool failure?

Result:

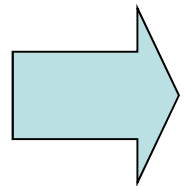
The prediction of tooling failure is still not a standard application of simulation.

Successful applications allowed to find out guidelines to support the design engineer based on reliable simulation results.

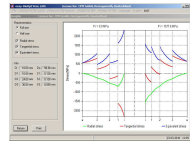
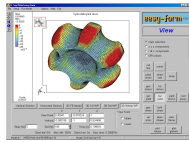
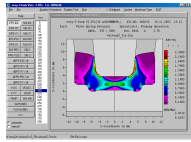
By getting experience from the studies rules could be given to enable the design engineer to foresee problems and therefore avoid costs.

The design engineer is enabled to develop longer lasting tooling by using simulation instead of costly trial and error procedures.

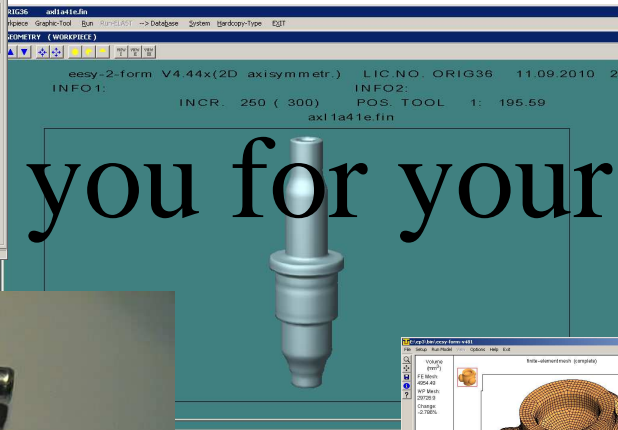
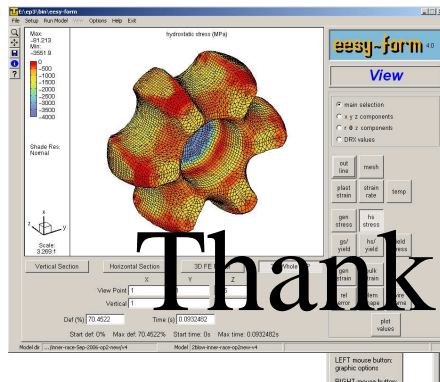
The study focused on real applications in industry and gave most practical guidelines.



The research has to go on to provide more sound and reliable models on a higher level to better predict not only tool failure but tool life as well.



Study of FEA applications in metal forming



Thank you for your attention

